



Patent  
Attorney's Docket No. 024444-818



IN THE UNITED STATES PATENT AND TRADEMARK OFFICE

UTILITY PATENT  
APPLICATION TRANSMITTAL LETTER

Box PATENT APPLICATION

Assistant Commissioner for Patents  
Washington, D.C. 20231

Sir:

Enclosed for filing is the utility patent application of Anders JONSSON, Anders PIIRHONEN, Torbjörn SELINDER and Gregor KULLANDER for COATED GROOVING OR PARTING INSERT AND METHOD OF MAKING SAME.

Also enclosed are:

- ☒ one sheet(s) of ☒ formal ☐ informal drawing(s);
- ☒ a claim for foreign priority under 35 U.S.C. §§ 119 and/or 365 is ☒ hereby made to 9903089-2 filed in Sweden on September 1, 1999; ☒ in the declaration;
- ☐ a certified copy of the priority document;
- ☐ a General Authorization for Petitions for Extensions of Time and Payment of Fees;
- ☐ \_\_\_\_\_ statement(s) claiming small entity status;
- ☐ an Assignment document;
- ☐ an Information Disclosure Statement; and
- ☐ Other: \_\_\_\_\_.
- ☒ An ☐ executed ☒ unexecuted declaration of the inventor(s) ☒ also is enclosed ☐ will follow.
- ☐ Please amend the specification by inserting before the first line the sentence --This application claims priority under 35 U.S.C. §§119 and/or 365 to \_ filed in \_ on \_; the entire content of which is hereby incorporated by reference.--
- ☐ A bibliographic data entry sheet is enclosed.



21839

☒ The filing fee has been calculated as follows ☐ and in accordance with the enclosed preliminary amendment:

C L A I M S					
	NO. OF CLAIMS		EXTRA CLAIMS	RATE	FEE
Basic Application Fee					\$690.00 (101)
Total Claims	6	MINUS 20 =	0	x \$18.00 (103)	--
Independent Claims	2	MINUS 3 =	0	x \$78.00 (102)	--
If multiple dependent claims are presented, add \$260.00 (104)					
Total Application Fee					\$690.00
If verified Statement claiming small entity status is enclosed, subtract 50% of Total Application Fee					
Add Assignment Recording Fee if Assignment document is enclosed					
<b>TOTAL APPLICATION FEE DUE</b>					<b>\$690.00</b>

- ☐ This application is being filed without a filing fee. Issuance of a Notice to File Missing Parts of Application is respectfully requested.
- ☒ A check in the amount of \$ 690.00 is enclosed for the fee due.
- ☐ Charge \$ \_\_\_\_\_ to Deposit Account No. 02-4800 for the fee due.
- ☒ The Commissioner is hereby authorized to charge any appropriate fees under 37 C.F.R. §§ 1.16, 1.17 and 1.21 that may be required by this paper, and to credit any overpayment, to Deposit Account No. 02-4800. This paper is submitted in duplicate.

Please address all correspondence concerning the present application to:

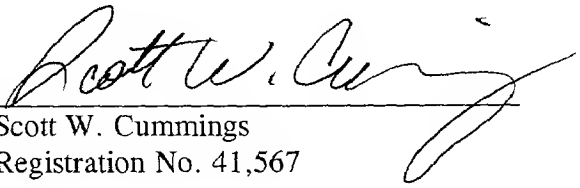
Ronald L. Grudziecki, Esq.  
Burns, Doane, Swecker & Mathis, L.L.P.  
P.O. Box 1404  
Alexandria, Virginia 22313-1404.

Respectfully submitted,

BURNS, DOANE, SWECKER & MATHIS, L.L.P.

Date: August 31, 2000

By:

  
\_\_\_\_\_  
Scott W. Cummings  
Registration No. 41,567

P.O. Box 1404  
Alexandria, Virginia 22313-1404  
(703) 836-6620

Attorney's Docket No. 024444-818

Utility Patent Application

for

COATED GROOVING OR PARTING INSERT  
AND METHOD OF MAKING SAME

by

ANDERS JONSSON, AHNDERS PIIRHONEN,  
TORBJÖRN SELINDER and GREGOR KULLANDER

BURNS, DOANE, SWECKER & MATHIS, L.L.P.  
Post Office Box 1404  
Alexandria, Virginia 22313-1404  
Telephone: (703) 836-6620

Date: August 31, 2000

**COATED GROOVING OR PARTING INSERT AND METHOD OF MAKING SAME**

**BACKGROUND OF THE INVENTION**

Field of the Invention:

5           The present invention relates to a coated cutting tool (cemented carbide insert) useful for grooving or parting of steel components, such as bars or tubes, not only of stainless steels of different compositions and microstructures but also of non-stainless steels such as low carbon steels and low and medium alloyed steels.

Description of Related Art:

10           In the discussion of the state of the art that follows, reference is made to certain structures and/or methods. However, the following references should not be construed as an admission that these structures and/or methods constitute prior art. Applicant expressly reserves the right to demonstrate that such structures and/or methods do not qualify as prior art against the present invention.

15           When machining low and medium alloyed steels and stainless steels with cemented carbide tools, the cutting edge is worn according to different wear mechanisms. Examples of such mechanisms include chemical wear, abrasive wear, adhesive wear and edge chipping. In bad cutting conditions problems with bulk and edge line breakages commonly occur. Furthermore, different cutting variables, such as cutting speed and cutting feed rate, and external conditions,  
20           such as dry or wet machining and heavy vibrations of the work piece, require a plurality of different properties of the cutting edge.

          It has been very difficult to improve all of the plurality of preferred tool properties simultaneously. Therefore, commercial cemented carbide grades have been optimized with respect to one or only a few of these wear types and, hence, to specific application areas.

US 6,062,776 discloses a coated cutting insert particularly useful for dry and wet machining in low and medium alloyed steels and stainless steels, with or without raw surface zones, under severe conditions such as vibration, long overhang, and recutting of chips. The insert is characterized by a WC-Co cemented carbide with a low content of cubic carbides, a rather low W-alloyed binder phase, and a coating including an innermost layer of  $\text{TiC}_x\text{N}_y\text{O}_z$  with columnar grains and a top layer of TiN and an inner layer of  $\kappa\text{-Al}_2\text{O}_3$ .

Swedish patent application SE 9901149-6 discloses a coated cutting insert, particularly useful at high cutting speeds, for use on stainless steels of different compositions and microstructures. The insert is also useful for the milling of non-stainless steels such as low carbon steels and low and medium alloyed steels. The coated WC-Co based cemented carbide insert is characterized by a specific composition range of WC/Co without any addition of cubic carbides, a low W-alloyed Co binder, a narrowly defined range of average WC grainsizes, and a hard and wear resistant coating including a multilayered structure of sublayers of the composition  $(\text{Ti}_x\text{Al}_{1-x})\text{N}$  with repeated variation of the Ti/Al ratio.

## SUMMARY OF THE INVENTION

It has now surprisingly been found that a combination of a modified cemented carbide substrate described in the above mentioned US 6,062,776 and the coating described in the above mentioned SE 9901149-6 results in excellent cutting performance in grooving or, in particular, parting of steel, including stainless steel.

A cutting tool insert, for parting of steel and stainless steel, and a method of making the same is provided. The cutting tool insert is comprised of a cemented carbide body and a coating wherein the cemented carbide body consists of WC with an average grain size of about 1.4  $\mu\text{m}$ , 12-13 wt-% Co, 0.4-1.8 wt-% TaC+NbC, and a low W-alloyed binder phase with a CW-ratio of

0.82-0.91. The coating is comprised of a multiple layers. The first (innermost) layer is 0.1-0.5  $\mu\text{m}$  of TiN. A second layer is comprised of a multilayered structure of 0.05-0.2  $\mu\text{m}$  thick sublayers. The sublayers are of a composition  $(\text{Ti}_x\text{Al}_{1-x})\text{N}$  in which x varies repeatedly between the two ranges  $0.45 < x < 0.55$  and  $0.70 < x < 0.80$ . A first sublayer, adjacent to the TiN bonding layer, is of a composition  $(\text{Ti}_x\text{Al}_{1-x})\text{N}$  having an x-value of  $0.45 < x < 0.55$ . A second sublayer is of a composition  $(\text{Ti}_x\text{Al}_{1-x})\text{N}$  having an x-value of  $0.70 < x < 0.80$  and a third sublayer is of a composition  $(\text{Ti}_x\text{Al}_{1-x})\text{N}$  having x of  $0.45 < x < 0.55$ . The sequence of sublayers alternates and repeats until 12-25 sublayers are built up. After the multilayered structure, a third layer of  $(\text{Ti}_x\text{Al}_{1-x})\text{N}$ , where x is  $0.45 < x < 0.55$ , is deposited to a thickness of 0.1-0.5  $\mu\text{m}$ . A fourth and outermost layer of TiN is deposited to a thickness of 0.1-0.2  $\mu\text{m}$ . The total coating thickness is 1-8 mm and the thickness of the second layer constitutes 75-95% of the total coating thickness.

## BRIEF DESCRIPTION OF THE DRAWING FIGURE

The objects and advantages of the invention will become apparent from the following detailed description of preferred embodiments thereof in connection with the accompanying drawings in which like numerals designate like elements and in which:

Figure 1 is a micrograph of a polished cross section of a coated insert according to the present invention.

## DETAILED DESCRIPTION OF PREFERRED EMBODIMENTS

Fig. 1 shows a micrograph at 1200X magnification of a polished cross section of a coated insert according to the present invention in which the layers of the cross section are visible. The layers are a cemented carbide body **A**, an innermost TiN layer **B**, a layer of several TiAlN sublayers **C**, a layer of TiAlN **D**, and an outermost TiN layer **E**.

According to the present invention, there is provided a coated cutting tool insert that satisfies the toughness demands of machining operations such as the grooving and parting of stainless steels. The coated cutting tool insert comprises a WC-Co based cemented carbide body with a composition of 11.5-13.6 wt% Co, preferably 12.0-13.0 wt% Co, most preferably 12.3-12.9 wt% Co, 0.2-1.8 wt% cubic carbides, preferably 0.4-1.8 wt% cubic carbides, most preferably 0.5-1.7 wt% cubic carbides of the metals Ta, Nb and Ti and balance WC. The cemented carbide may also contain other carbides from elements from group IVb, Vb or VIb of the periodic table. The content of Ti is preferably on a level corresponding to a technical impurity. The average grain size of the WC is about 1.1-2.1  $\mu\text{m}$ , preferably about 1.4  $\mu\text{m}$ .

The cobalt binder phase is rather low and alloyed with W. The content of W in the binder phase can be expressed as the CW-ratio:

$$\text{CW-ratio} = M_s / (\text{wt\% Co} \cdot 0.0161) \quad (1)$$

where  $M_s$  is the saturation magnetization of the cemented carbide body in kA/m and wt% Co is the weight percentage of Co in the cemented carbide. The CW-value is a function of the W content in the Co binder phase. A high CW-value corresponds to a low W-content in the binder phase.

It has now been found according to the present invention that improved cutting performance is achieved if the cemented carbide body has a CW-ratio of 0.80-0.92, preferably 0.82-0.91, and most preferably 0.85-0.90. The cemented carbide may contain small amounts, < 1 volume %, of  $\eta$ -phase ( $\text{M}_6\text{C}$ ), without any detrimental effect. From the CW-value it follows that no free graphite is allowed in the cemented carbide body according to the present invention.

The hard and wear resistant refractory coating deposited on the cemented carbide substrate A according to the present invention comprises a first (innermost) thin 0.1-0.5  $\mu\text{m}$  bonding layer of TiN B.



The coating includes a second layer comprising a multilayered structure of sublayers C of the composition  $(\text{Ti}_x\text{Al}_{1-x})\text{N}$  in which x varies repeatedly between the two ranges  $0.45 < x < 0.55$  and  $0.70 < x < 0.80$ . The first sublayer of  $(\text{Ti}_x\text{Al}_{1-x})\text{N}$  adjacent to the TiN bonding layer having an x-value of  $0.45 < x < 0.55$ , the second sublayer of  $(\text{Ti}_x\text{Al}_{1-x})\text{N}$  having an x-value of  $0.70 < x < 0.80$  and the third sublayer having x of  $0.45 < x < 0.55$  and so forth repeated until 12-25 sublayers, preferably 22-24 sublayers, are built up. The thickness of this second layer comprising a multilayered structure of sublayers constitutes 75-95 % of the total coating thickness. The individual sublayers of  $(\text{Ti}_x\text{Al}_{1-x})\text{N}$  are essentially of the same thickness but their thickness may also vary in a regular or irregular way and said sublayer thickness is 0.05-0.2  $\mu\text{m}$ .

The coating further includes a third 0.1-0.5  $\mu\text{m}$  layer of  $(\text{Ti}_x\text{Al}_{1-x})\text{N}$  D having an x-value of  $0.45 < x < 0.55$ , and a fourth (outermost) thin 0.1-0.2  $\mu\text{m}$  layer of TiN E.

The total thickness of the coating is 1-8  $\mu\text{m}$ , preferably 2-5  $\mu\text{m}$ . The layer thickness, the sublayer thickness and the coating thickness quoted above refer to measurements made close to the cutting edge, i.e. - the functional part of the cutting tool.

The present invention will now be further described by reference to the following examples, which are intended to be illustrative rather restrictive.

#### Example 1

A. A cemented carbide parting tool insert in accordance with the present invention with a composition of 12.6 wt-% Co, 1.25 wt-% TaC, 0.30 wt-% NbC and balance WC with a 1.4  $\mu\text{m}$  grain size and with a binder phase alloyed with W corresponding to a CW-ratio of 0.91 was coated with a 4  $\mu\text{m}$  thick coating by applying a conventional PVD cathodic arc technique. The coating consisted of a first (innermost) 0.2  $\mu\text{m}$  layer of TiN followed by a 3.2  $\mu\text{m}$  thick second layer comprising 23 alternating sublayers of  $(\text{Ti}_x\text{Al}_{1-x})\text{N}$ , where x alternatively varied between

0.55 and 0.75, a third layer  $0.2 \mu\text{m}$   $(\text{Ti}_x\text{Al}_{1-x})\text{N}$ , where  $x = 0.55$ , and, finally, an outermost  $0.4 \mu\text{m}$  layer of TiN.

B. A cemented carbide parting tool insert not of the present invention with a composition of 8.0 wt-% Co, no cubic carbides, balance WC and a CW-ratio of 0.94. The insert was coated  
5 with an innermost  $0.5 \mu\text{m}$  equiaxed TiCN-layer. A  $1.5 \mu\text{m}$  TiN layer was deposited, during the same cycle, on top of the TiCN-layer. No post treatment was applied.

C. For comparison, a competitive cemented carbide parting tool insert in style similar to previously mentioned inserts was obtained from an external leading cemented carbide producer. The carbide had a composition of 12.5 wt-% Co, 0.1 wt-% TiC, 1.8 wt-% TaC, 0.2 wt-% NbC,  
10 and balance WC with a CW-ratio of 0.87. The insert had a coating consisting of  $1.4 \mu\text{m}$  TiN and, outermost,  $1.4 \mu\text{m}$  TiCN. Examination under a light optical microscope revealed no edge treatment subsequent to coating.

Inserts A, B and C were tested in a parting off to center in stainless steel SS2321 with OD  
15 26 mm. The cutting speed was varied from 86 to 0 m/min with a feed rate of 0.05 mm/r. The wear mechanism was uneven flank wear and chipping.

	<u>Insert</u>	<u>Number of components</u>
	A	50
20	B	13
	C	41

#### Example 2

Inserts A and B were tested at an end user's machine shop in a parting of a stainless steel  
25 component (AISI 316 OD 42 mm). The cutting speed was varied from 110 to 0 m/min with a

feed rate varying from 0.08 to 0.03 mm/r. The low feed rate was used close to the center of the bar. The wear mechanism was fracture in the cutting zone.

	<u>Insert</u>	<u>Number of components</u>
5	A	201
	B	224

### Example 3

Inserts A and B were tested at an end user's machine shop in a parting of a steel component (SS2172 OD 47 mm). The rotating speed was 1800 rpm with a feed rate of 0.1 mm/r. The wear mechanism was flank wear and flaking.

	<u>Insert</u>	<u>Number of components</u>
	A	163
15	B	50

### Example 4

Inserts A and C were tested at an end user's machine shop in a parting of a stainless steel component (AISI 316 OD 31 mm). The cutting speed was varied from 60 to 0 m/min with a feed rate varying from 0.06 to 0.03 mm/r. The low feed rate was used close to the center of the bar. The wear mechanism was flank wear and chipping.

<u>Insert</u>	<u>Number of components</u>
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A	182
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C	43
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5       The present invention also relates to a method of making a coated cutting tool insert consisting of a cemented carbide body with a composition of 11.5-13.6 wt% Co, preferably 12.0-13.0 wt% Co, most preferably 12.3-12.9 wt% Co, 0.2-1.8 wt% cubic carbides, preferably 0.4-1.8 wt% cubic carbides, most preferably 0.5-1.7 wt% cubic carbides of the metals Ta, Nb and Ti and balance WC. The cemented carbide may also contain other carbides from elements from group IVb, Vb or VIb of the periodic table. The content of Ti is preferably on a level corresponding to a technical impurity. The average grain size of the WC is about 1.1-2.1  $\mu\text{m}$ , preferably about 1.4  $\mu\text{m}$ .

10       The hard and wear resistant refractory coating is deposited onto the cemented carbide substrate by applying conventional PVD (Physical Vapor Deposition) or CVD (Chemical Vapor Deposition) methods and, according to the present invention, said coating comprises a first  
15       (innermost) thin 0.1-0.5  $\mu\text{m}$  bonding layer of TiN, a second layer comprising a multilayered structure of sublayers of the composition  $(\text{Ti}_x\text{Al}_{1-x})\text{N}$  in which x varies repeatedly between the two ranges  $0.45 < x < 0.55$  and  $0.70 < x < 0.80$ . The first sublayer of  $(\text{Ti}_x\text{Al}_{1-x})\text{N}$  adjacent to the TiN bonding layer having an x-value of  $0.45 < x < 0.55$ , the second sublayer of  $(\text{Ti}_x\text{Al}_{1-x})\text{N}$   
20       having an x-value of  $0.70 < x < 0.80$  and the third sublayer having x of  $0.45 < x < 0.55$  and so forth repeated until 12-25 sublayers, preferably 22-24 sublayers, are built up. The thickness of this second layer comprising a multilayered structure of sublayers constitutes 75-95% of the total coating thickness. The individual sublayers of  $(\text{Ti}_x\text{Al}_{1-x})\text{N}$  are essentially of the same thickness but their thickness may also vary in a regular or irregular way and said sublayer thickness is

Although the present invention has been described in connection with preferred  
embodiments thereof, it will be appreciated by those skilled in the art that additions, deletions,  
5 modifications, and substitutions not specifically described may be made without department from  
the spirit and scope of the invention as defined in the appended claims.

[illegible]

**WHAT IS CLAIMED IS:**

1. A cutting tool comprising:

a cemented carbide body comprising WC with an average grain size of about  $1.4\ \mu\text{m}$ , 12-13 wt-% Co, 0.4-1.8 wt-% TaC+NbC, and a low W-alloyed binder phase with a CW-ratio of 0.82-0.91; and

a coating comprising:

- a first innermost  $0.1\text{-}0.5\ \mu\text{m}$  thick layer of TiN;

- a second layer comprising a multilayered structure of  $0.05\text{-}0.2\ \mu\text{m}$  thick sublayers of a composition  $(\text{Ti}_x\text{Al}_{1-x})\text{N}$  in which x varies repeatedly between the two ranges

$0.45 < x < 0.55$  and  $0.70 < x < 0.80$ , a first sublayer of  $(\text{Ti}_x\text{Al}_{1-x})\text{N}$  adjacent to the TiN

bonding layer having an x-value of  $0.45 < x < 0.55$ , a second sublayer of  $(\text{Ti}_x\text{Al}_{1-x})\text{N}$

having an x-value of  $0.70 < x < 0.80$  and a third sublayer having x of  $0.45 < x < 0.55$ , the sequence of sublayers alternating and repeating until 12-25 sublayers are built up;

- a third  $0.1\text{-}0.5\ \mu\text{m}$  thick layer of  $(\text{Ti}_x\text{Al}_{1-x})\text{N}$ , where x is  $0.45 < x < 0.55$ ; and

- a fourth outermost  $0.1\text{-}0.2\ \mu\text{m}$  layer of TiN;

wherein the total coating thickness is  $1\text{-}8\ \mu\text{m}$  and the thickness of the second layer constitutes 75-95% of the total coating thickness.

2. The cutting tool according to claim 1 wherein the cemented carbide body has a composition comprising 12.3-12.9 wt-% Co and 0.5-1.7 wt% TaC+NbC.

3. The cutting tool according to claim 1 wherein the cemented carbide body is free from graphite.

4. A method of making a cutting tool, the cutting tool comprising a WC-Co based cemented carbide body comprising WC with an average grain size of about  $1.4\ \mu\text{m}$ , 12-13 wt-% Co and 0.4-1.8 wt-% TaC+NbC, and a low W-alloyed binder phase with a CW-ratio of 0.82-0.91, the method comprising:

5       - applying by PVD a first innermost  $0.1\text{-}0.5\ \mu\text{m}$  bonding layer of TiN to the body;  
      - applying by PVD a second layer comprising a multilayered structure comprising a plurality of  $0.05\text{-}0.2\ \mu\text{m}$  thick sublayers of a composition  $(\text{Ti}_x\text{Al}_{1-x})\text{N}$  in which x varies repeatedly between the two ranges  $0.45 < x < 0.55$  and  $0.70 < x < 0.80$ , a first sublayer of  $(\text{Ti}_x\text{Al}_{1-x})\text{N}$  adjacent to the TiN bonding layer having an x-value of  $0.45 < x < 0.55$ , a second sublayer of  $(\text{Ti}_x\text{Al}_{1-x})\text{N}$  having an x-value of  $0.70 < x < 0.80$  and a third sublayer having x in the range  $0.45 < x < 0.55$ , the sequence of sublayers alternating and repeating until 12-25 sublayers are built up;

      - applying by PVD a third  $0.1\text{-}0.5\ \mu\text{m}$  thick layer of  $(\text{Ti}_x\text{Al}_{1-x})\text{N}$ , where x is  $0.45 < x < 0.55$ ; and

15       - applying by PVD a fourth outermost  $0.1\text{-}0.2\ \mu\text{m}$  layer of TiN;  
      wherein the total coating thickness close to a cutting edge of the tool is in the range of  $1\text{-}8\ \mu\text{m}$  and the thickness of the second layer constitutes 75-95% of the total coating thickness,

5. The method according to claim 4 wherein the cemented carbide body comprises a WC-Co composition of WC with an average grain size of about  $1.4\ \mu\text{m}$ , 12-13 wt-% Co and 0.4-1.8 wt-% TaC+NbC, and a low W-alloyed binder phase with a CW-ratio of 0.82-0.91.

6. The method according to claim 4 wherein the wear resistant coating is deposited by CVD techniques.

The present invention relates to a coated cutting tool (e.g. - cemented carbide insert) useful for grooving or parting of steel or stainless steel components such as tubes and bars. The insert is characterised by a WC-Co-based cemented carbide substrate having a highly W-alloyed Co-binder phase and a hard and wear resistant coating including a multilayered structure of sublayers of the composition  $(\text{Ti}_x\text{Al}_{1-x})\text{N}$  with a periodic and repeated variation of the Ti/Al ratio.



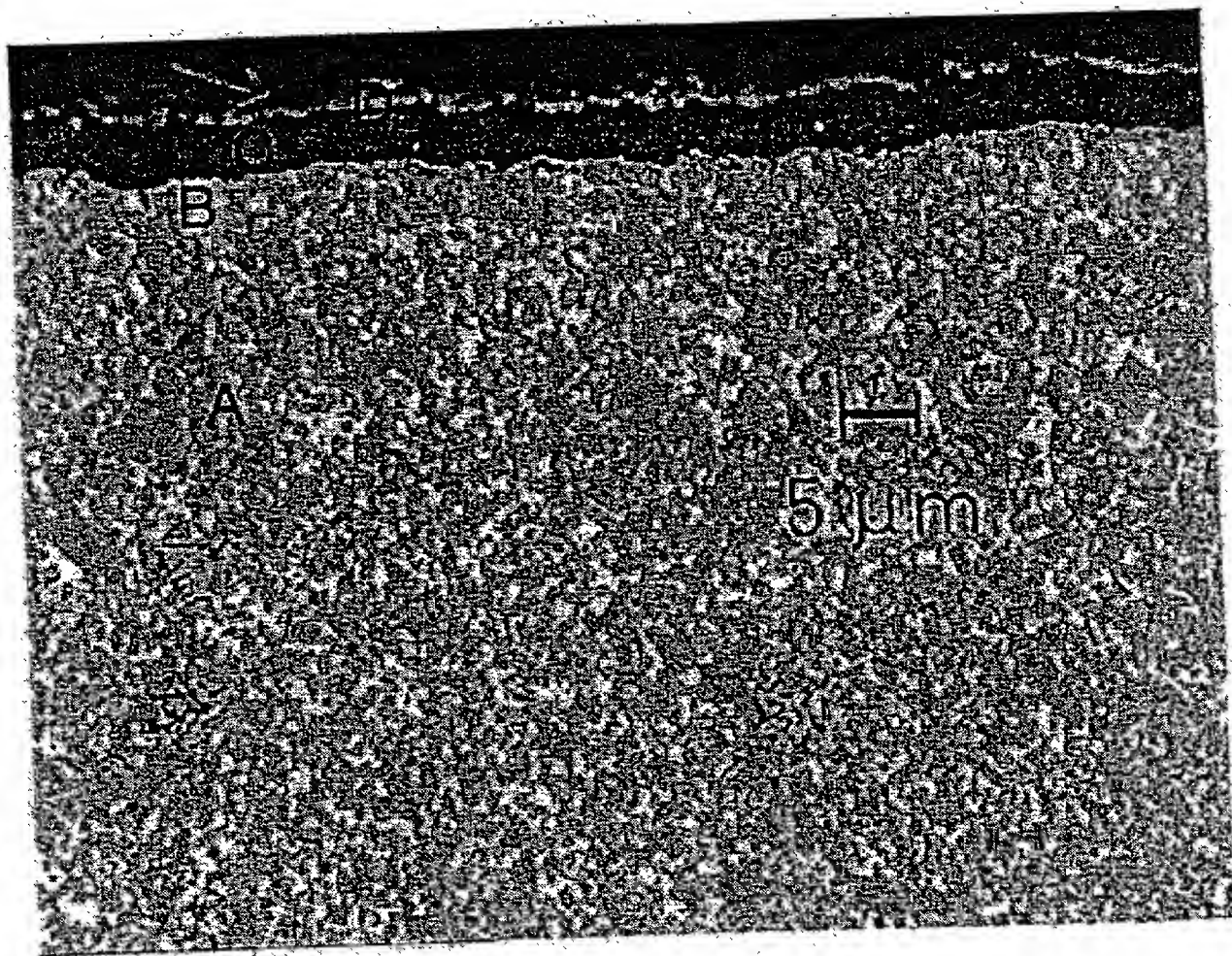


Fig. 1

**COMBINED DECLARATION AND POWER OF ATTORNEY  
FOR UTILITY PATENT APPLICATION**

Attorney's Docket No.  
024444-818

As a below-named inventor, I hereby declare that:

My residence, post office address and citizenship are as stated below next to my name;

I BELIEVE I AM THE ORIGINAL, FIRST AND SOLE INVENTOR (if only one name is listed below) OR AN ORIGINAL, FIRST AND JOINT INVENTOR (if more than one name is listed below) OF THE SUBJECT MATTER WHICH IS CLAIMED AND FOR WHICH A PATENT IS SOUGHT ON THE INVENTION ENTITLED:

COATED GROOVING OR PARTING INSERT AND METHOD OF MAKING SAME

the specification of which

(check one)

☒ is attached hereto;

☐ was filed on \_\_\_\_\_ as

Application No. \_\_\_\_\_

and was amended on \_\_\_\_\_;  
(if applicable)

I HAVE REVIEWED AND UNDERSTAND THE CONTENTS OF THE ABOVE-IDENTIFIED SPECIFICATION, INCLUDING THE CLAIMS, AS AMENDED BY ANY AMENDMENT REFERRED TO ABOVE;

I ACKNOWLEDGE THE DUTY TO DISCLOSE TO THE OFFICE ALL INFORMATION KNOWN TO ME TO BE MATERIAL TO PATENTABILITY AS DEFINED IN TITLE 37, CODE OF FEDERAL REGULATIONS, Sec. 1.56 (as amended effective March 16, 1992);

I do not know and do not believe the said invention was ever known or used in the United States of America before my or our invention thereof, or patented or described in any printed publication in any country before my or our invention thereof or more than one year prior to said application; that said invention was not in public use or on sale in the United States of America more than one year prior to said application; that said invention has not been patented or made the subject of an inventor's certificate issued before the date of said application in any country foreign to the United States of America on any application filed by me or my legal representatives or assigns more than twelve months prior to said application;

I hereby claim foreign priority benefits under Title 35, United States Code Sec. 119 and/or Sec. 365 of any foreign application(s) for patent or inventor's certificate as indicated below and have also identified below any foreign application for patent or inventor's certificate on this invention having a filing date before that of the application(s) on which priority is claimed:

## COMBINED DECLARATION AND POWER OF ATTORNEY

Attorney's Docket No.  
024444-818

COUNTRY/INTERNATIONAL	APPLICATION NUMBER	DATE OF FILING (day, month, year)	PRIORITY CLAIMED
SWEDEN	9903089-2	01-09-99	YES <input checked="" type="checkbox"/> NO <input type="checkbox"/>
			YES <input type="checkbox"/> NO <input type="checkbox"/>

I hereby appoint the following attorneys and agent(s) to prosecute said application and to transact all business in the Patent and Trademark Office connected therewith and to file, prosecute and to transact all business in connection with international applications directed to said invention:

William L. Mathis	17,337	R. Danny Huntington	27,903	Gerald F. Swiss	30,113
Robert S. Swecker	19,885	Eric H. Weisblatt	30,505	Michael J. Ure	33,089
Platon N. Mandros	22,124	James W. Peterson	26,057	Charles F. Wieland III	33,096
Benton S. Duffett, Jr	22,030	Teresa Stanek Rea	30,427	Bruce T. Wieder	33,815
Norman H. Stepno	22,716	Robert E. Krebs	25,885	Todd R. Walters	34,040
Ronald L. Grudziecki	24,970	William C. Rowland	30,888	Ronni S. Jillions	31,979
Frederick G. Michaud, Jr.	26,003	T. Gene Dillahunt	25,423	Harold R. Brown III	36,341
Alan E. Kopecki	25,813	Patrick C. Keane	32,858	Allen R. Baum	36,086
Regis E. Slutter	26,999	Bruce J. Boggs, Jr.	32,344	Steven M. du Bois	35,023
Samuel C. Miller, III	27,360	William H. Benz	25,952	Brian P. O'Shaughnessy	32,747
Robert G. Mukai	28,531	Peter K. Skiff	31,917	Kenneth B. Leffler	36,075
George A. Hovanec, Jr.	28,223	Richard J. McGrath	29,195	Fred W. Hathaway	32,236
James A. LaBarre	28,632	Matthew L. Schneider	32,814		
E. Joseph Gess	28,510	Michael G. Savage	32,596		



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and: Scott W. Cummings, Registration No. 41,567

Address all correspondence to:



21839

Ronald L. Grudziecki  
BURNS, DOANE, SWECKER & MATHIS, L.L.P.  
P.O. Box 1404  
Alexandria, Virginia 22313-1404

Address all telephone calls to: Scott W. Cummings 836-6620.

I hereby declare that all statements made herein of my own knowledge are true and that all statements made on information and belief are believed to be true; and further that these statements were made with the knowledge that willful false statements and the like so made are punishable by fine or imprisonment, or both, under Section 1001 of Title 18 of the United States Code and that such willful false statements may jeopardize the validity of the application or any patent issued thereon.

FULL NAME OF SOLE OR FIRST INVENTOR	SIGNATURE	DATE
Anders JONSSON		
RESIDENCE	CITIZENSHIP	
Gävle, SWEDEN	SWEDEN	
POST OFFICE ADDRESS		
Kvisttorpsbacken 6, 804 27, Gävle, SWEDEN		
FULL NAME OF SECOND JOINT INVENTOR, IF ANY	SIGNATURE	DATE
Anders PIIRHONEN		
RESIDENCE	CITIZENSHIP	
Sandviken, SWEDEN	SWEDEN	
POST OFFICE ADDRESS		
Coromantgatan 12D, 811 54 Sandviken, SWEDEN		

<b>COMBINED DECLARATION AND POWER OF ATTORNEY</b>	Attorney's Docket No. 024444-818
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FULL NAME OF THIRD JOINT INVENTOR, IF ANY Torbjörn SELINDER	SIGNATURE	DATE
RESIDENCE Stockholm SWEDEN	CITIZENSHIP SWEDEN	
POST OFFICE ADDRESS Katrinebergsbacken 18, 117 61 Stockholm SWEDEN		
FULL NAME OF FOURTH JOINT INVENTOR, IF ANY Gregor KULLANDER	SIGNATURE	DATE
RESIDENCE Älvsjö, SWEDEN	CITIZENSHIP SWEDEN	
POST OFFICE ADDRESS Långsjöhöjden 79, 125 51 Älvsjö, SWEDEN		

024444-818